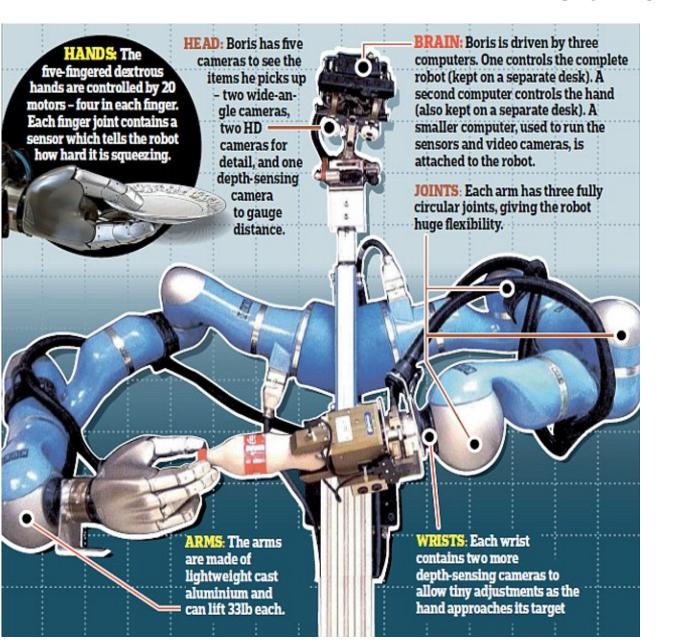
# Automated Design of Special Purpose Dexterous Manipulators

Christopher Hazard

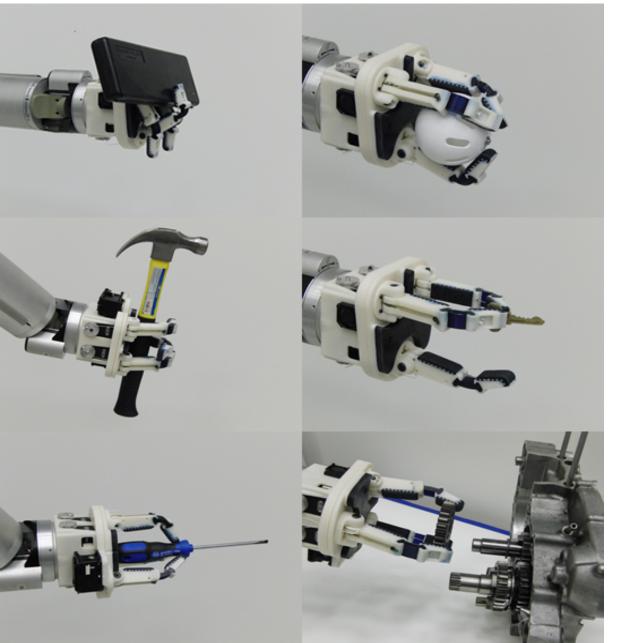
#### Motivation

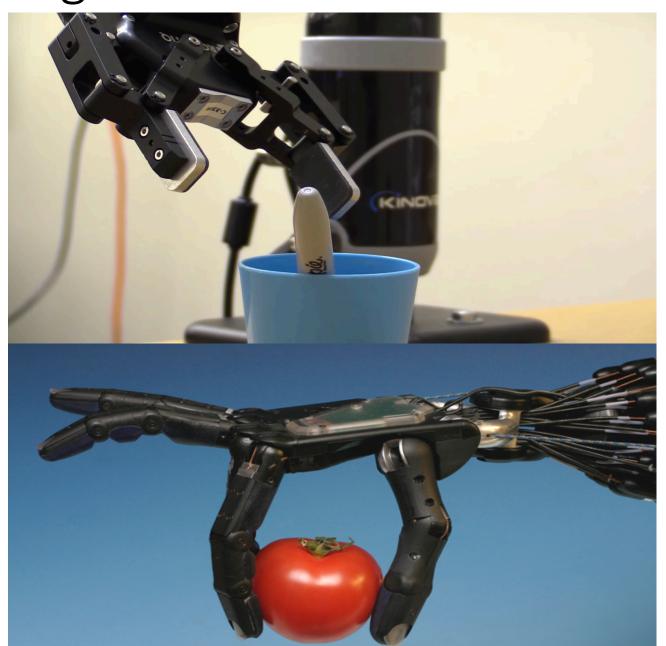






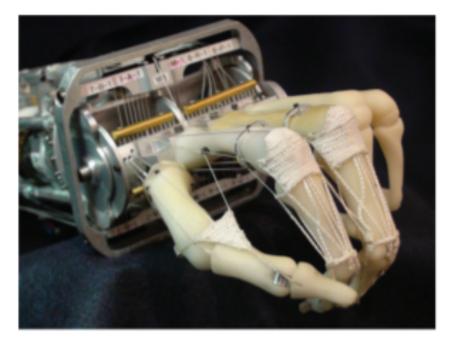
## Challenges



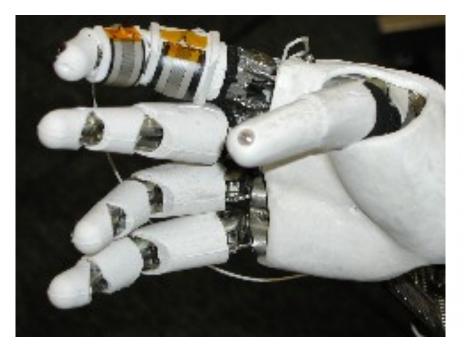


#### **Humanoid Hands**

- Goal: mirror human hand
- Impressive capability
- Important limitations
- Very expensive
- Costly mechanical failures



ACT: anatomically correct testbed hand



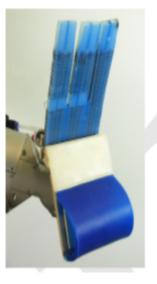
NASA Robonaut Hand

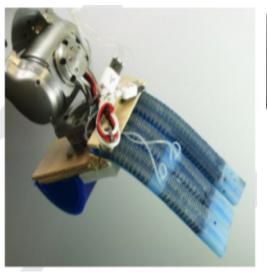


**Shadow Dexterous** 

- [1] "The ACT hand: Design of the skeletal structure" Weghe 2004
- [2] "The robonaut hand: A dexterous robot hand for space" Lovchick 1999
- [3] Shadow Dexterous: https://www.shadowrobot.com

## Low Cost (Simplified) Hands







Pneumatic Hand (Diemel 2013)

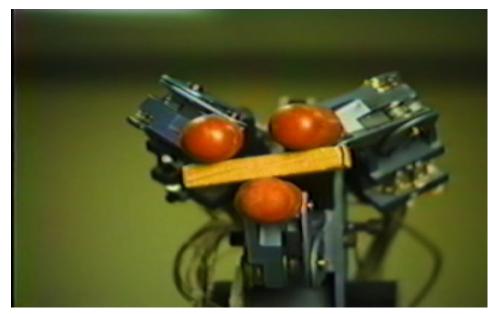
3D printed Hand (Ma 2013)

SDM Hand (Dollar 2010)

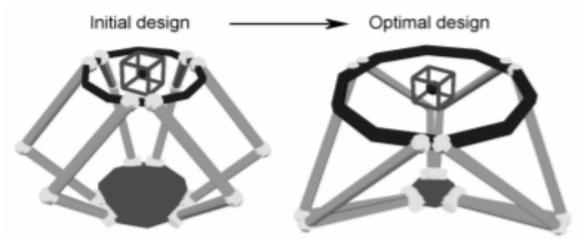
- underactuated designs
- 3d printable components
- cheap materials + simple construction
- soft/compliant components
- cheap embedded sensing

- [1] "A modular, open-source 3D printed underactuated hand" Ma 2013
- [2] "A compliant hand based on a novel pneumatic actuator" Deimel 2013
- [3] "The highly adaptive SDM hand: Design and performance evaluation" Dollar 2010

#### Design Parameter Optimization



Salisbury 1982: Stanford-JPL hand



Collard 2005: Manipulability Optimization

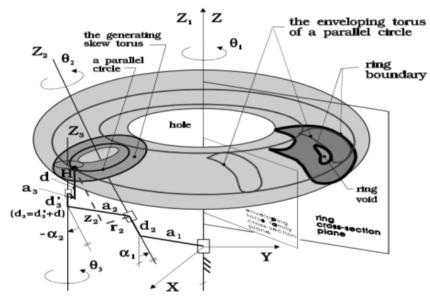
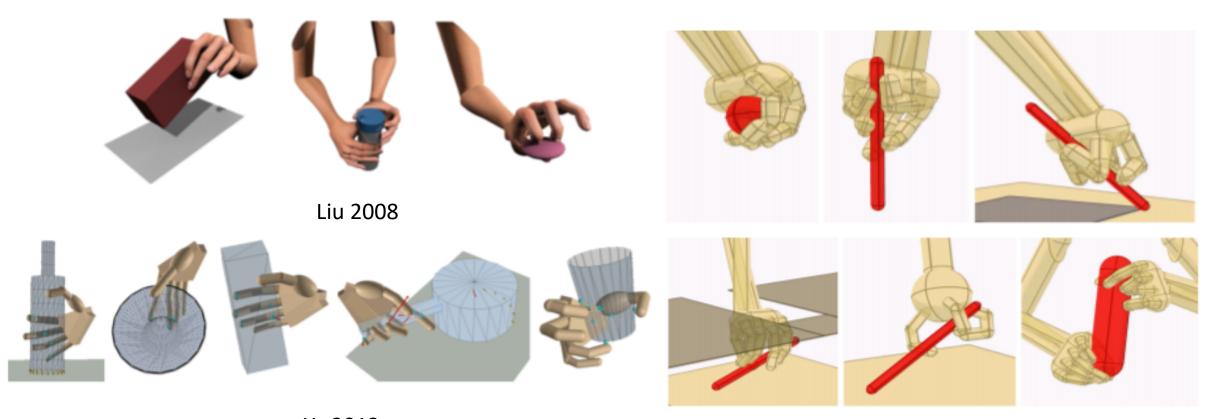


Fig. 2. Design parameters and workspace geometry for 3R manipulators.

Ceccarelli 2004: workspace optimization

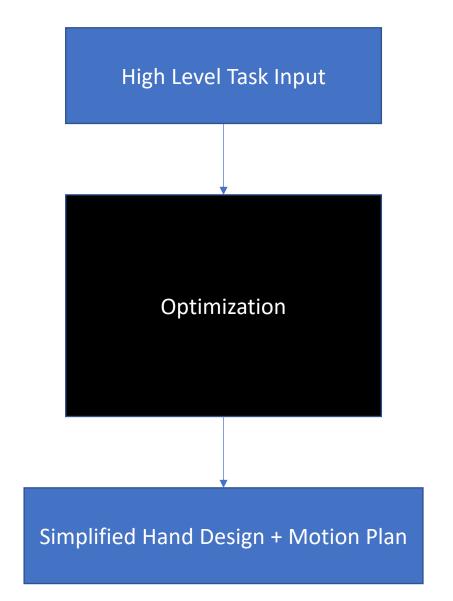
- [1] "Articulated hands: Force control and kinematic issues" Salisbury 1982
- [2] "A multi-objective optimum design of general 3R manipulators for prescribed workspace limits" Ceccarelli 2004
- [3] "Contribution to the optimization of closed-loop multibody systems: Application to parallel manipulators" Collard 2005
- [4]" An optimization problem approach for designing both serial and parallel manipulators" Ceccarelli 2005

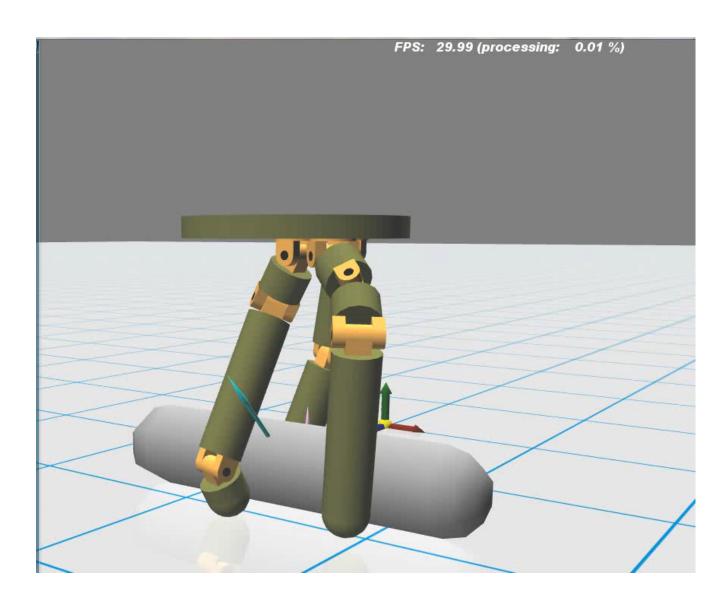
## Trajectory Optimization

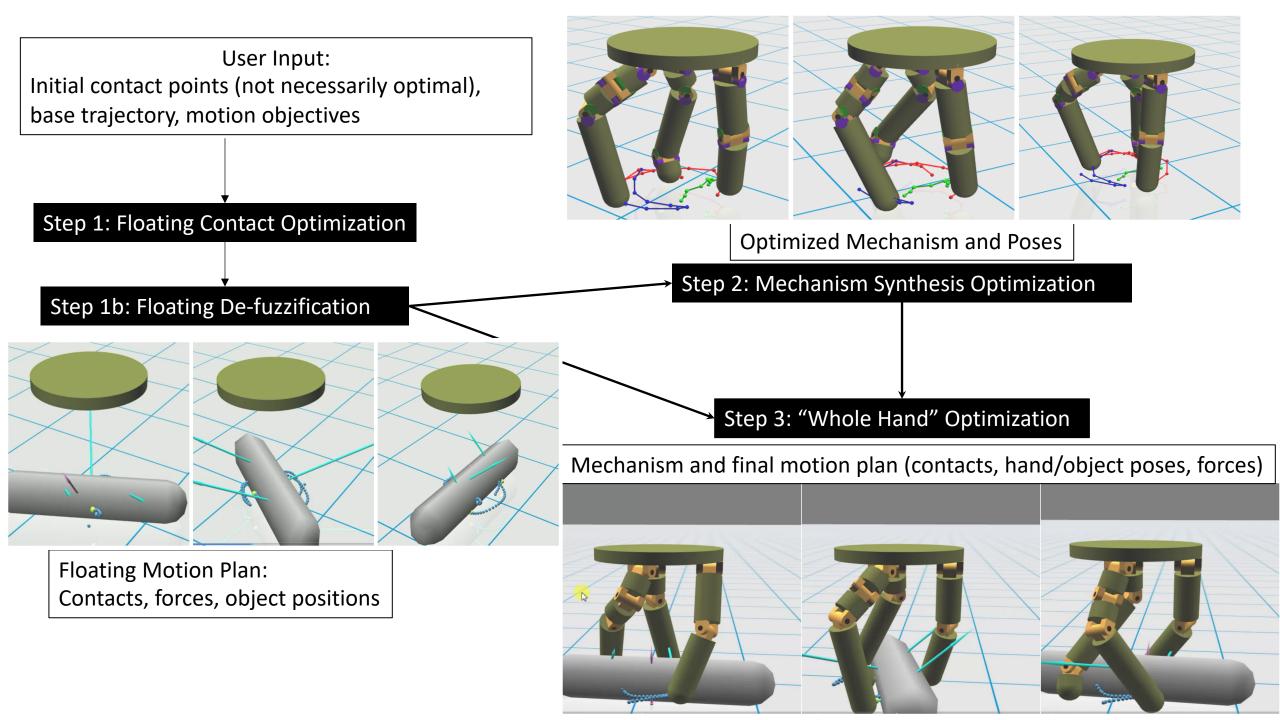


- Ye 2012 Mordatch 2012
- [1] "Construction and animation of anatomically based human hand models" Albrecht 2003
- [2] "Synthesis of interactive hand manipulation." Liu 2008
- [3] "Dextrous manipulation from a grasping pose" liu 2009
- [4] "Synthesis of Detailed Hand Manipulations Using Contact Sampling" Ye 2012
- [5] "Contact-invariant optimization for hand manipulation." Mordatch 2012

#### Our Work







# Step 1: Floating Contact Optimization

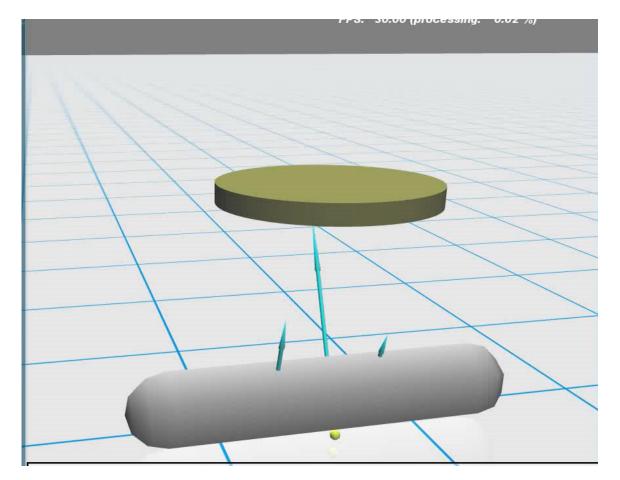
## Floating Contact Optimization

#### Input:

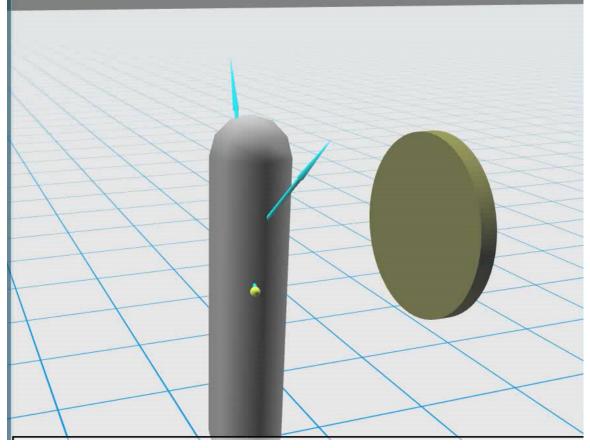
- Object goal poses
- Initial contact points

#### Output:

- Physically valid motion plan (contacts and forces)







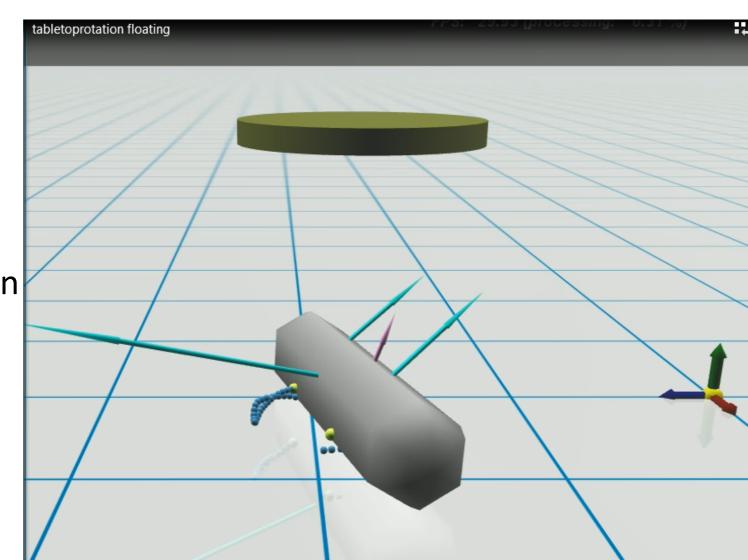
Vertical Flip

## Step 1: Floating Optimization Problem

$$\mathbf{S} = \underset{\mathbf{S}}{\operatorname{argmin}} \ \Sigma_t \Sigma_i \ w_i * L_i(t)$$
s.t.  $c_j \in [0, 1] \ for \ 0 \le t \le T$ 

$$\mathbf{S_t} = [\mathbf{x_O} \ \mathbf{f_j} \ \mathbf{r_j} \ c_j]$$

- x<sub>O</sub> = object position + orientation
- f<sub>i</sub> = contact force (contact j)
- r<sub>i</sub> = contact position (contact j)
- c<sub>i</sub> = contact invariant term



## Step 1: Floating Optimization Objective Terms

Task----specify goal of the manipulation

Physics—force and torque balancing + friction cone constraints

Contact Invariant terms—projection of contacts onto object surface

Additional Regularization Terms—smooth out the motion

#### Task Objective Terms

$$L_{task} = \frac{1}{k} \sum_{k} ||p(k) - p_{goal}(k)||^2 + quatdist(o(k), o_{goal}(k))^2$$

- Main objective type: object pose
- Quatdist: angular distance between 2 orientations

#### Alternative/additional objectives:

- End effector tracking between object and target points
- Additional perturbing forces

$$L_{ceTracking}(t) = \sum_{i} ||p_{ce}(t) - p_{target}(t)||^{2}$$

#### Physics Terms

$$L_{physics}(t) = L_{linMomentum}(t) + L_{angMomentum}(t)$$

$$L_{linMomentum}(t) = \sum_{i} c_i(t) f_i - m\ddot{x}$$

Applied Force Derivative of linear momentum

$$L_{angMomentum}(t) = ||\Sigma_i \ c_i(t) * (r_i \times f_{i,local}) - (\omega \times (I_{object}^{local} \omega) + I\dot{\omega})||^2$$
 Applied Torque Derivative of angular momentum

- x = object position
- f<sub>j</sub> = contact force (contact j)
- r<sub>j</sub> = contact position (contact j)
- c<sub>i</sub> = contact invariant term

#### Force and Contact Related Terms

**Force Related Costs** 

$$L_{forceReg}(t) = \sum_{i} ||c_i(t)f_i||^2$$

$$L_{frictionCone}(t) = \sum c_i * \exp(\alpha(||f_{i,local} - n * (f_i \cdot n_i)|| - \mu f_i \cdot n_i)))$$

$$f_{tangent}$$

$$f_{normal}$$

**Contact Invariant Related Costs** 

$$L_{ci\_object}(t) = \sum_{i} c_i ||r_{proj} - r_i||^2$$

Contact Projection Distance onto Object

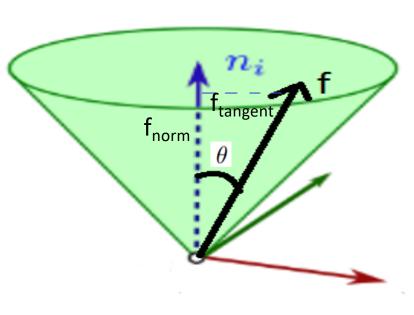
For contact i:

 $f_i$  = contact force

r<sub>i</sub> = contact position (object local frame)

 $n_i$  = object surface normal (local frame)

Alpha is a constant (sharpening factor)



 $J_{tangent} \le \mu J_{normal}$  i.e.

$$\theta = \tan^{-1} \frac{f_{tangent}}{f_{normal}} \le \tan^{-1} \mu$$

#### Additional Regularization Terms

$$L_{floatingContactAccel}(t) = \sum_{i} ||((r_i(t+t_{phys}) - 2*r_i(t) + r_i(t-t_{phys}))/(t_{phys}*t_{phys})||^2$$

Acceleration of contact: finite differences

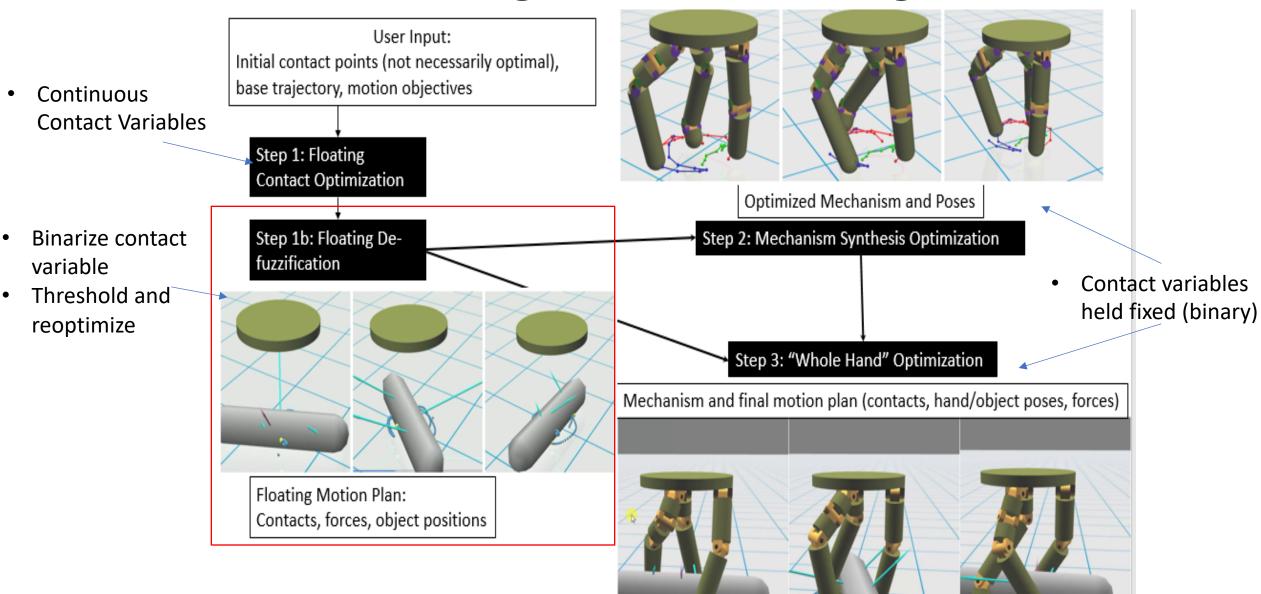
$$L_{accelerationRegularization}(t) = \sum_{i} \ddot{x}^{2}$$

Object acceleration: finite differences

$$L_{angular Acceleration Regularization}(t) = \sum_{i} (\omega \times (I_{world}\omega) + I_{world}\dot{\omega}/t_{phys})^{2}$$

Angular Momentum derivative

## Floating Post-Processing



# Step 2: Mechanism Synthesis

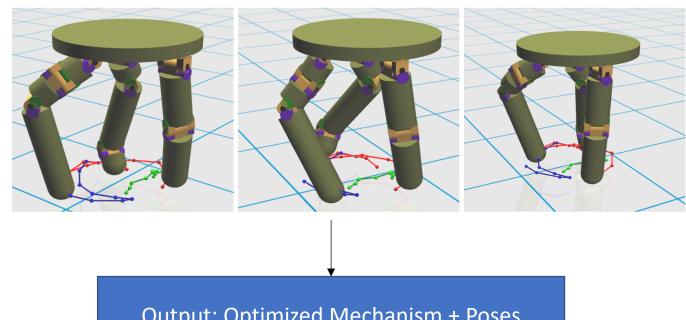
#### Step 2: Mechanism Synthesis

Contact **Motion Plan** Floating Optimization

Synthesis Optimization:

Joints per finger, joint axes, segment lengths, finger positions on base, hand poses

-Fingers track individual contact trajectories -Independently controlled joints



Output: Optimized Mechanism + Poses

#### Continuous Synthesis Optimization

$$\mathbf{M} = \underset{\mathbf{M}, \mathbf{Q}, \mathbf{P}}{\operatorname{argmin}} \Sigma_k \Sigma_i \ w_i * L_i(k)$$
  
for  $k \in \{1, 2, ..., N_{keyframes}\}$ 

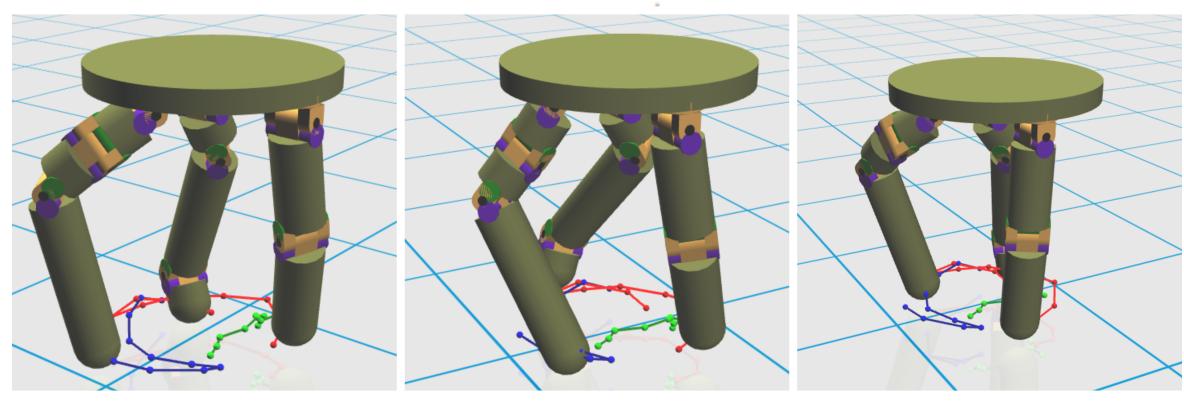
- Morphological parameters M:
  - -finger lengths
  - -joint axes
  - -locations of fingers on the base
- Joint positions Q (hand poses at each keyframe)
- Contact points P (on fingertips)

#### Synthesis Objective Terms

**Contact Point Costs** 

$$L_{eeTarget}(k) = \sum_{i} c_i * ||p_i - p_{target}||^2$$

$$L_{fingerContactDistSurface}(k) = \sum ||p_{proj} - p_i||^2$$

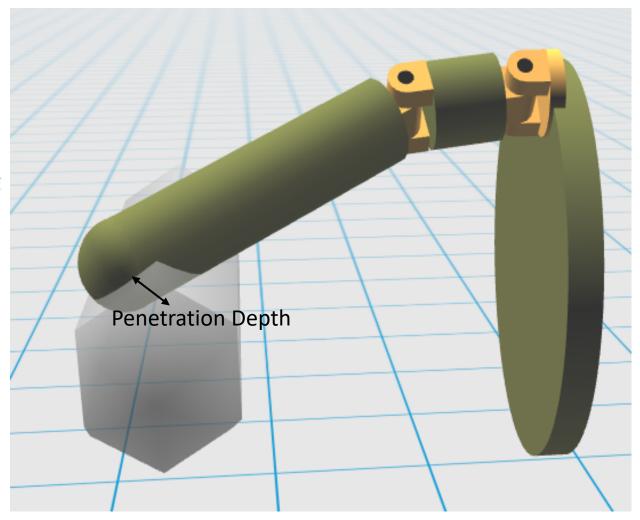


## Synthesis Objective Terms

#### **Collision Penalties**

$$g(x) = \begin{cases} 0 & x \le -\epsilon \\ \frac{x^3}{6\epsilon} + \frac{x^2}{2} + \frac{\epsilon x}{2} + \frac{\epsilon^2}{6} & -\epsilon \le x \le \epsilon \\ x^2 + \frac{\epsilon^2}{3} & \epsilon \le x \end{cases}$$

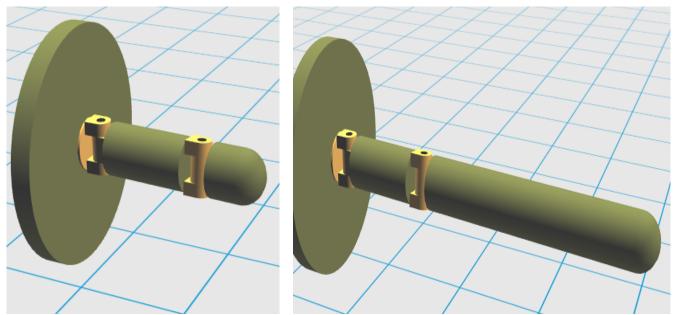
$$L_{collision}(k) = \sum_{i,j \in bodies} g(penetration(body_i, body_j))$$



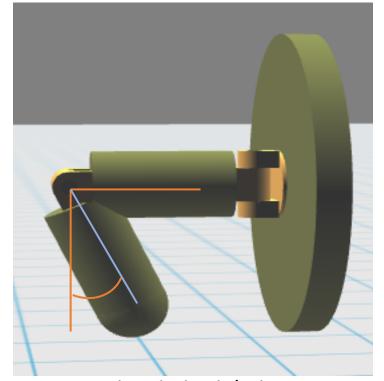
#### **Additional Costs**

$$L_{fingerLengthRegularization} == \sum_{i} (l_i)^2 \qquad L_{jointLimits}(k) = \sum_{i \in keyframes} \sum_{a \in joints} g(a(i) - a_{max}) + g(a_{min} - a(i))$$

$$L_{fingerMinLengthCost} = \sum_{i} g(l_{min} - l_i)$$



Distal link: min length and a large length

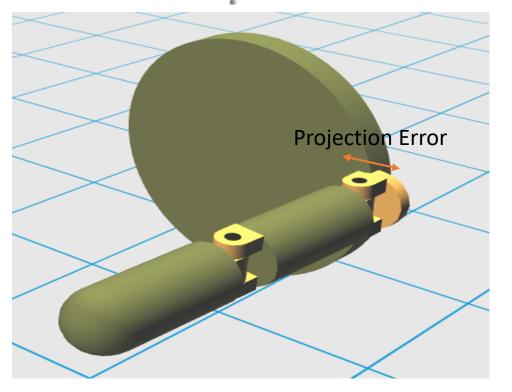


Joint Limit Violation

#### Additional Costs

$$L_{fingerAcceleration}(k) == \sum_{i} (1 - c_i) * \ddot{x_i}^2$$
  $L_{fingerPositions} = \sum_{i} ||proj_{base}(b_i) - b_i||)^2$ 

$$L_{fingerPositions} = \sum_{i} ||proj_{base}(b_i) - b_i||)^2$$



Lifted finger transitions smoothly from one side to the other

## Controllability Constraints

#### Jacobian Null Space:

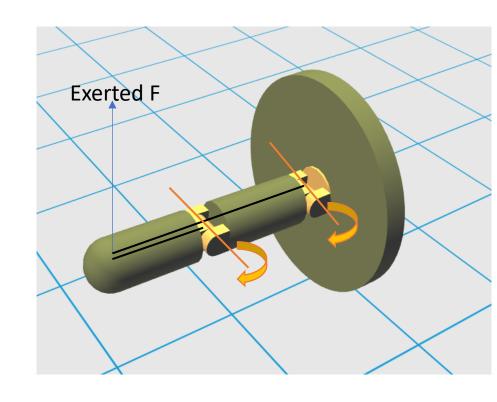
Let  $E = \{e_0, ..., e_k\}$  be an orthonormal basis of the Jacobian null space:

$$L_{jacNull} = \sum_{i} c_{i} * \sqrt{\sum_{k} (f \cdot e_{k})^{2}}$$

#### **Torque Regularization:**

$$F = T \times r_{perp} / ||r_{perp}||^2 + k * r_{perp}|$$

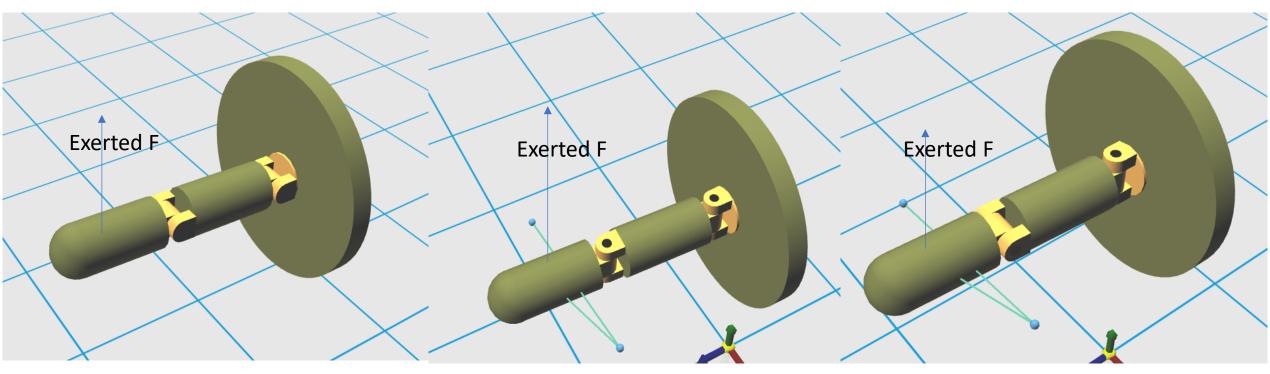
$$F = X * \alpha \longrightarrow \vec{\alpha} = (X^T X + \lambda^2 I)^{-1} X_T F$$



where X is the matrix consisting of column vectors  $T \times r_{perp} / ||r_{perp}||^2$ 

$$L_{torque} = \|\vec{\alpha}\|^2$$

#### Controllability Constraints Demonstration



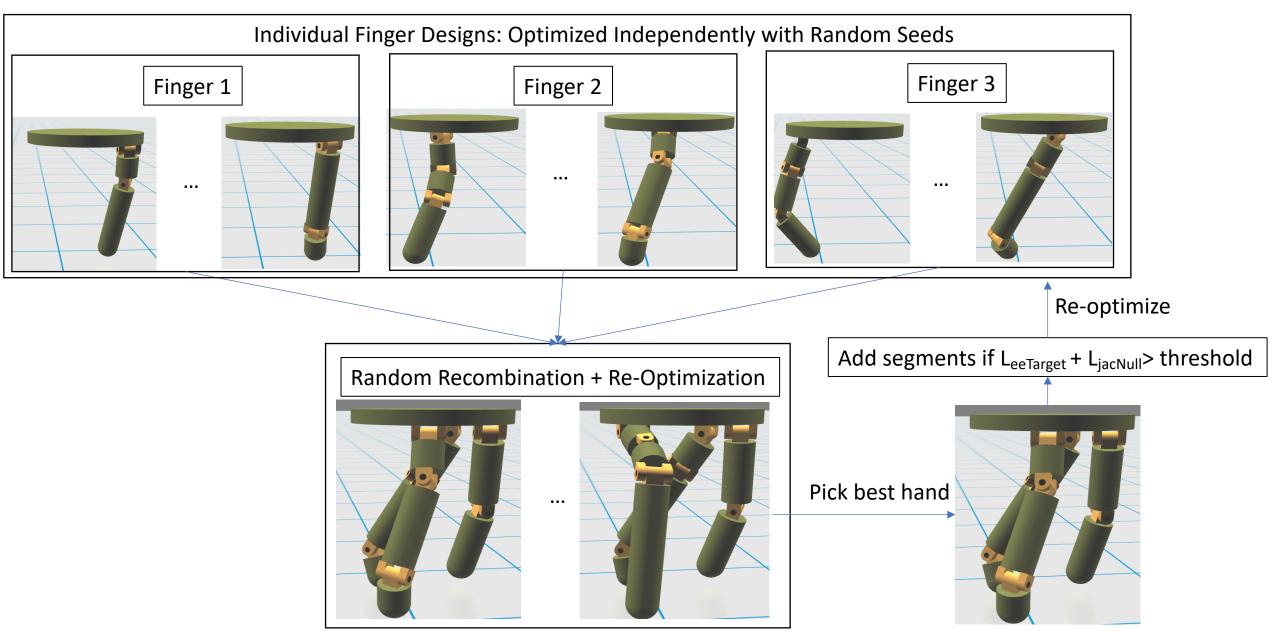
1. Finger held still: optimal joints

2. Finger rotates in plane Joints slightly off axis:

 $L_{jacNull} = 0$  $L_{torque}$  very high

3. Finger rotates in plane: Optimal joint configuration

## Synthesis Design Loop



# Step 3: Whole Hand Optimization

#### Whole Hand Optimization Problem

```
We wish to find a trajectory S = \{S_1, S_2, ..., S_{N_{keyframes}}\} such that

S = \underset{S}{\operatorname{argmin}} \Sigma_t \Sigma_i \ w_i * L_i(t)
s.t. c_j \in [0, 1] \ for \ 0 \le t \le T
```

- Adjusts the motion so it fits to the designed hand
- Uses floating objectives + additional objectives
- Also optimize for robot poses q
- Morphology stays fixed

## Additional Optimization Terms

Additional terms (from floating) adapted for hand:

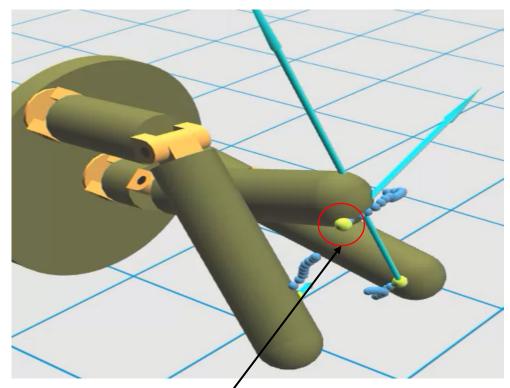
Contact projection onto fingertip surface

$$L_{ci\_finger}(t) = \sum_{i} c_i ||r_{proj} - r_i||^2$$

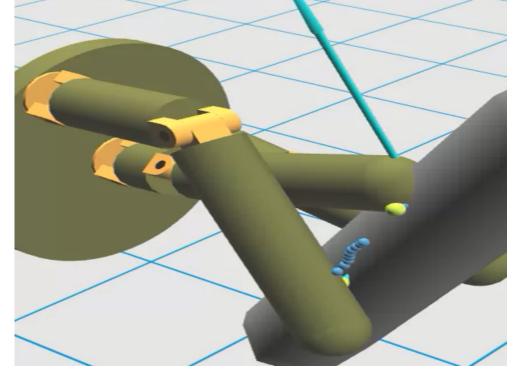
Friction Cone wrt fingertip surface

$$L_{frictionCone}(t) = \sum_{i} c_i * \exp(\alpha(||f_{i,local} - n * (f_i \cdot n_i)|| - \mu f_i \cdot n_i))$$

#### Hand Friction Cone Demonstration (without term)



Contact way outside friction cone w.r.t. finger



Caused by (small) errant collision with object

#### Additional Optimization Terms

Terms copied over from the synthesis step:

Controllability constraints

$$L_{jacNull} = \sum_{i} c_i * \sqrt{\sum_{k} (f \cdot e_k)^2}$$
$$L_{torque} = \|\vec{\alpha}\|^2$$

Collision (includes ground, hand, object, external objects)

$$L_{collision}(k) = \sum_{i,j \in bodies} g(penetration(body_i, body_j))$$

#### Other:

$$\begin{split} L_{fingerAcceleration}(k) =& = \sum_{i} (1 - c_i) * \ddot{x_i}^2 \\ L_{jointLimits}(k) = & \sum_{i \in keyframes} \sum_{a \in joints} g(a(i) - a_{max}) + g(a_{min} - a(i)) \end{split}$$

## Slippage Terms

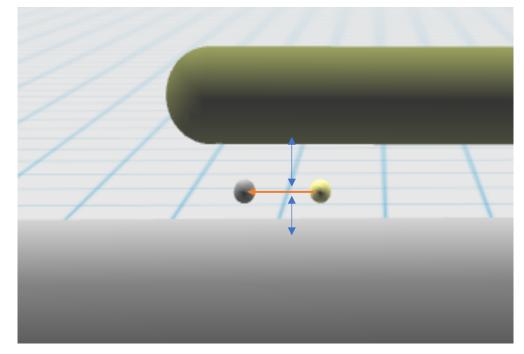
#### Slippage w.r.t. object

$$e_{object}(i, t) = r_{i,proj\_object}(t) - r_i(t)$$
  
 $L_{ci\_object\_slippage}(t) = \sum_{i} ||c_i f_i||^2 * ||(\dot{e}_{object}(i, t))||^2$ 

#### Slippage w.r.t. finger

$$e_{finger}(i, t) = r_{i,proj,finger}(t) - r_i(t)$$

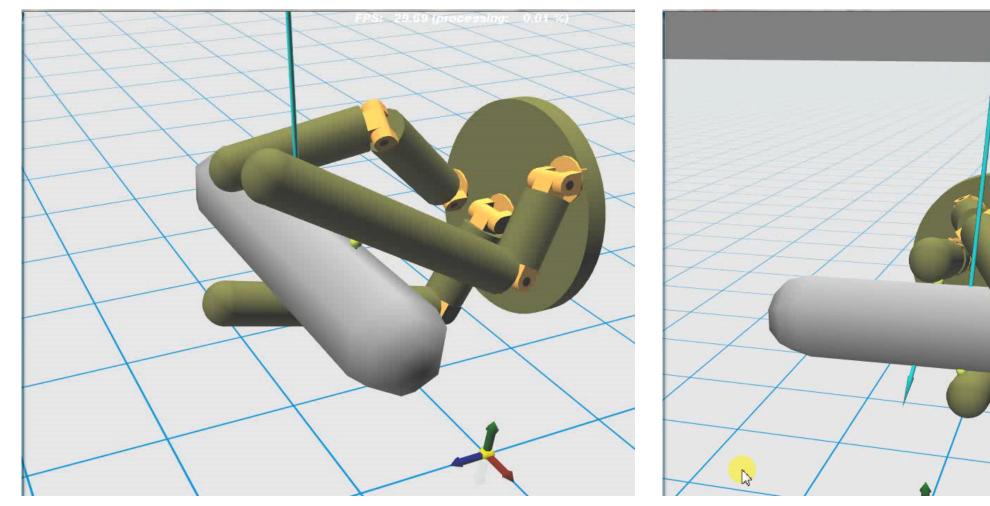
$$L_{ci\_finger\_slippage}(t) = \sum_{i} ||c_i f_i||^2 * ||(\dot{c}_{finger}(i, t))||^2$$

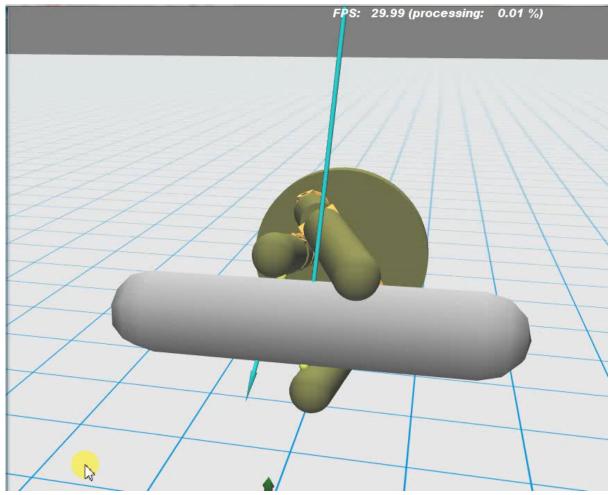


Zero slip penalty

Bottom Line: distance slipped on object = distance slipped on fingertip (w.r.t. world frame) Slip directions w.r.t world frame line up Not a complete model, but helpful

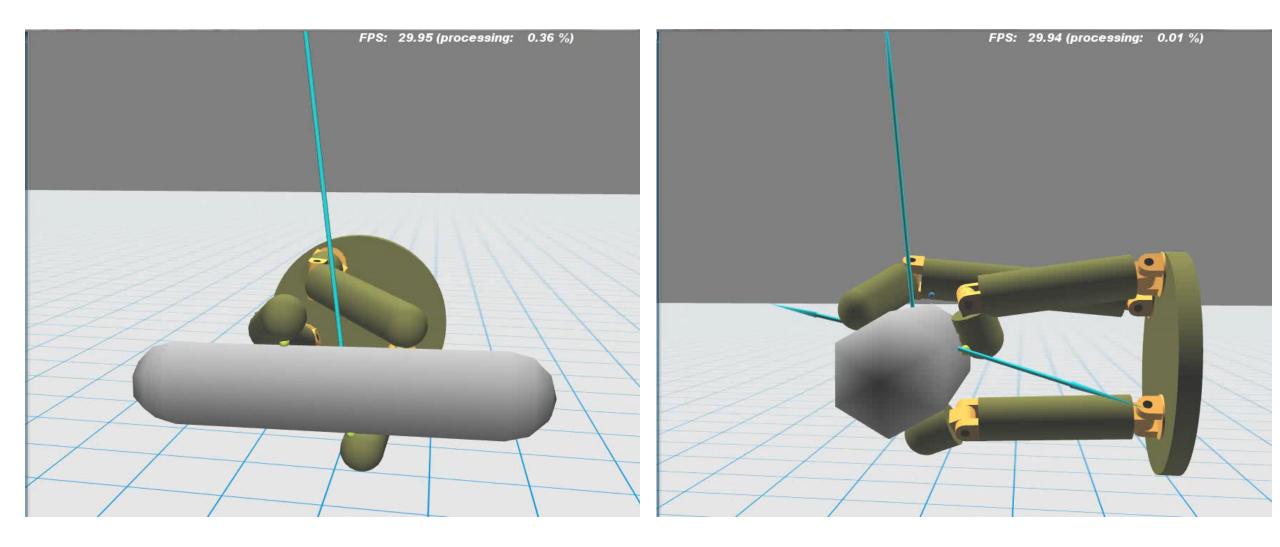
## Simple Manipulations





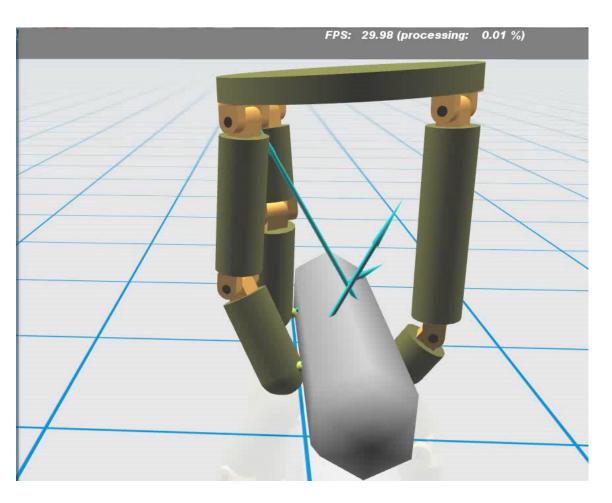
Translate **Vertical Rotate** 

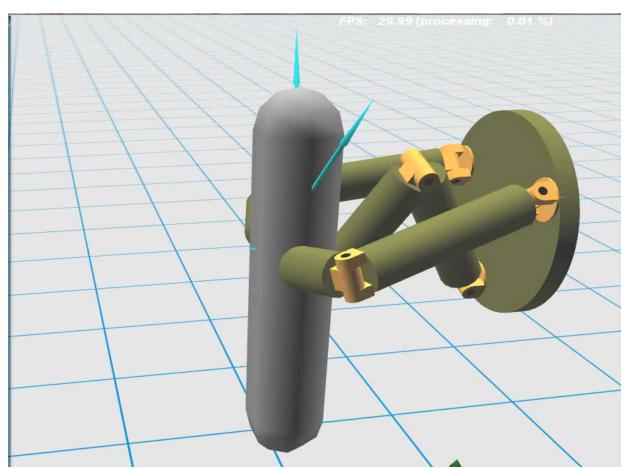
## Examples



180 Rotation Rotate and Bow Out

## More Examples

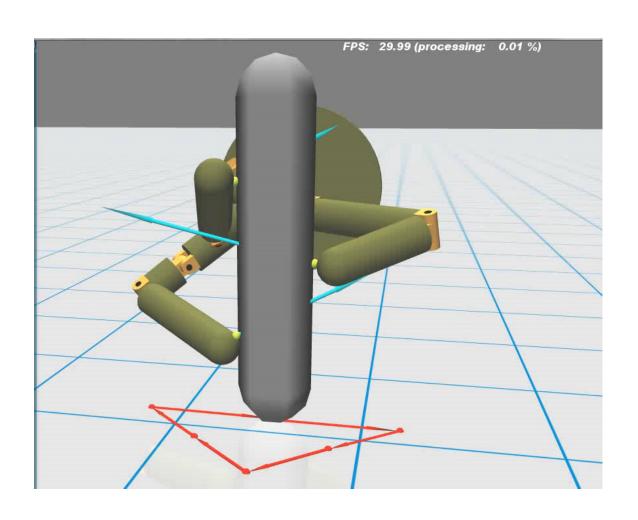


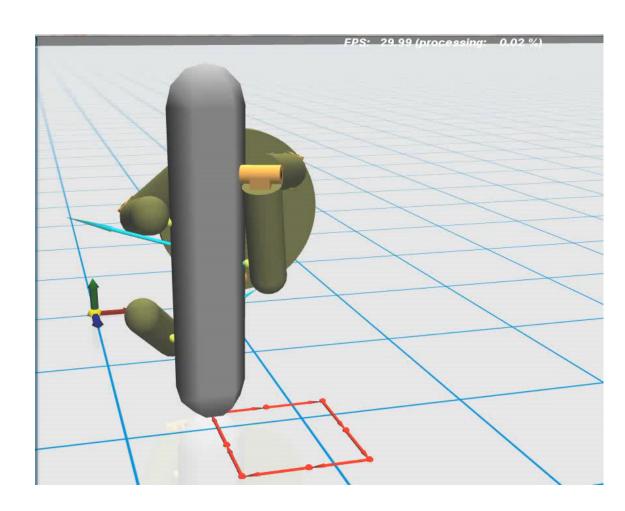


Pick up and rotate

Vertical flip

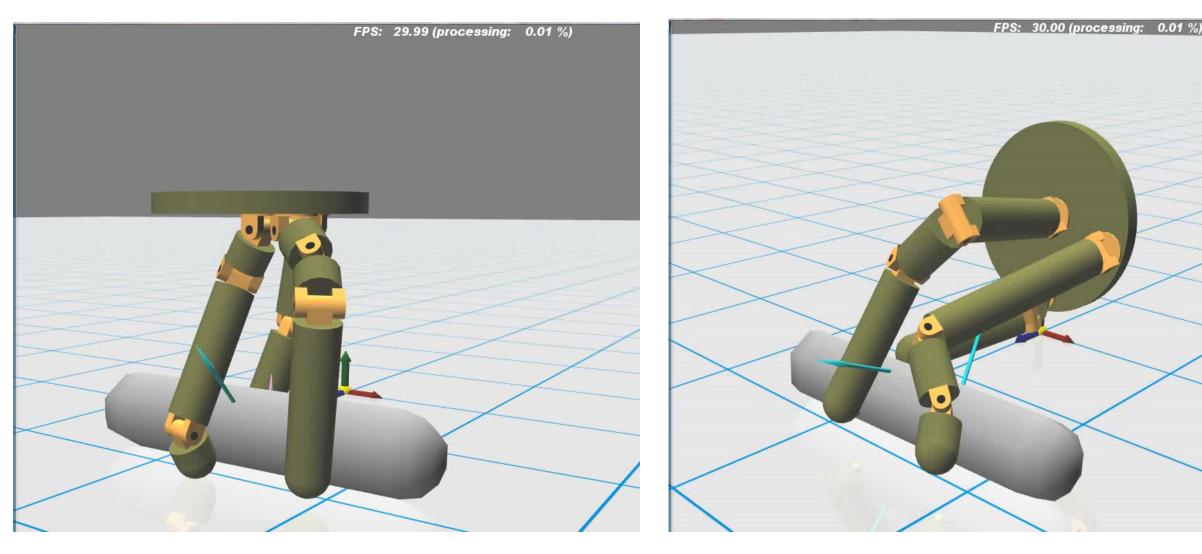
## Alternative Objective: Drawing





Draw triangle Draw box

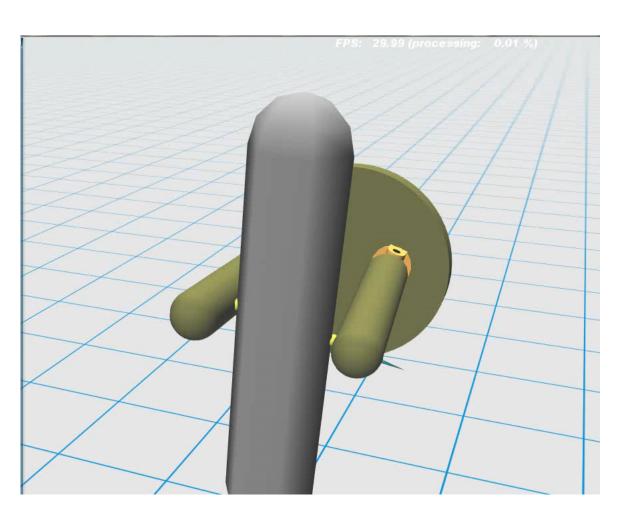
# Tabletop Rotation: Two versions

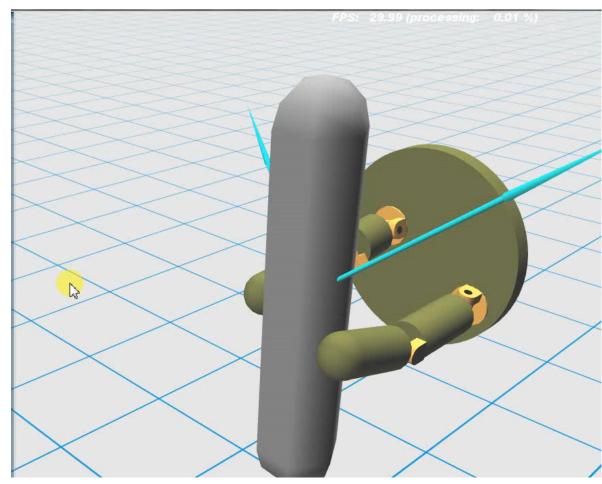


Tabletop from the side

Tabletop overtop

### Building Up a Motion From Primitives

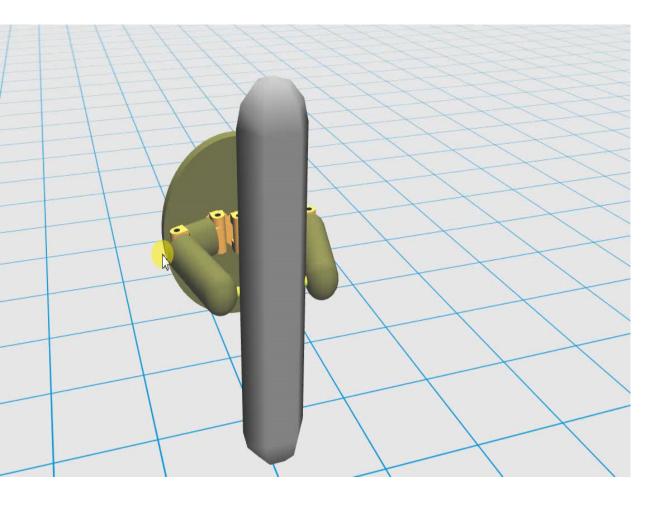




Horizontal (no gravity)

Horizontal (with gravity)

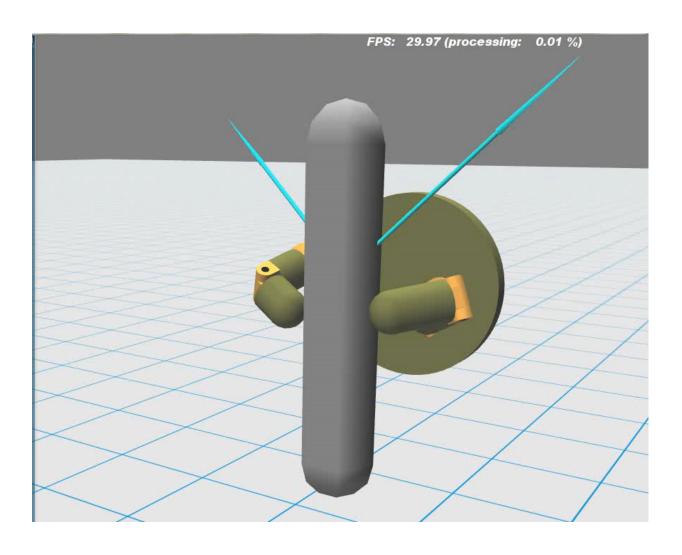
### Building Up a Motion From Primitives



Circle in plane (no gravity)

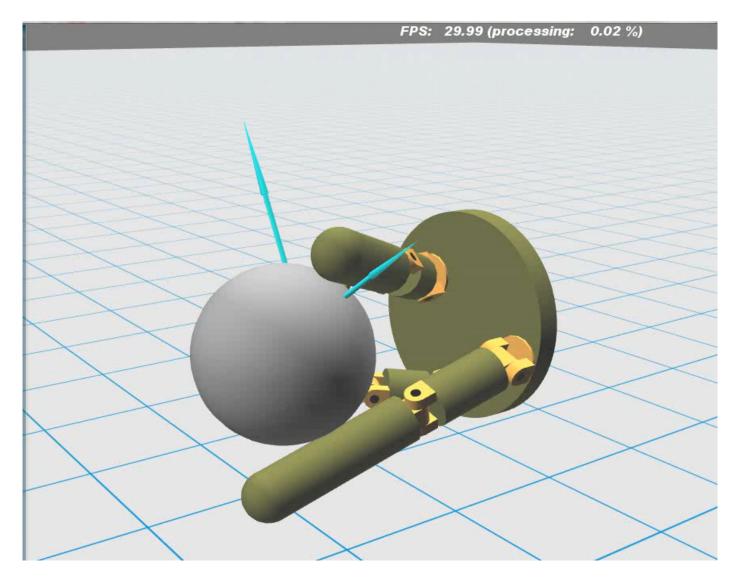
Circle in plane (with gravity)

## Building Up a Motion From Primitives



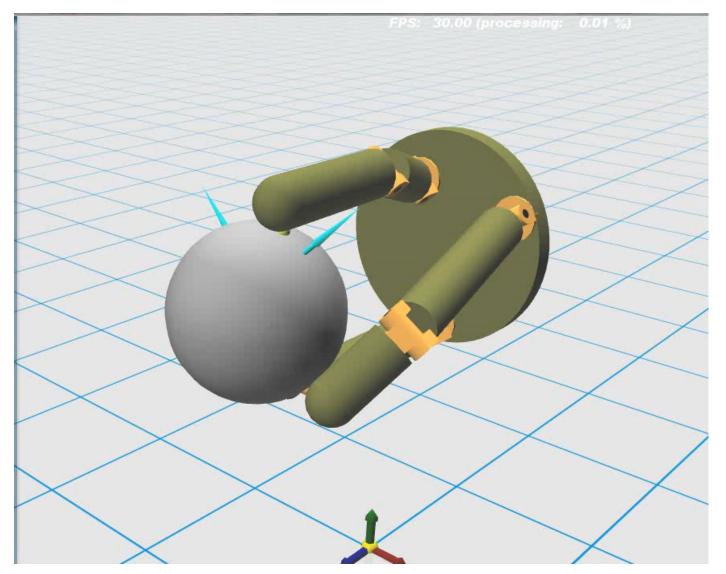
Hemisphere (with gravity)

## "Multi-objective" Chaining Example



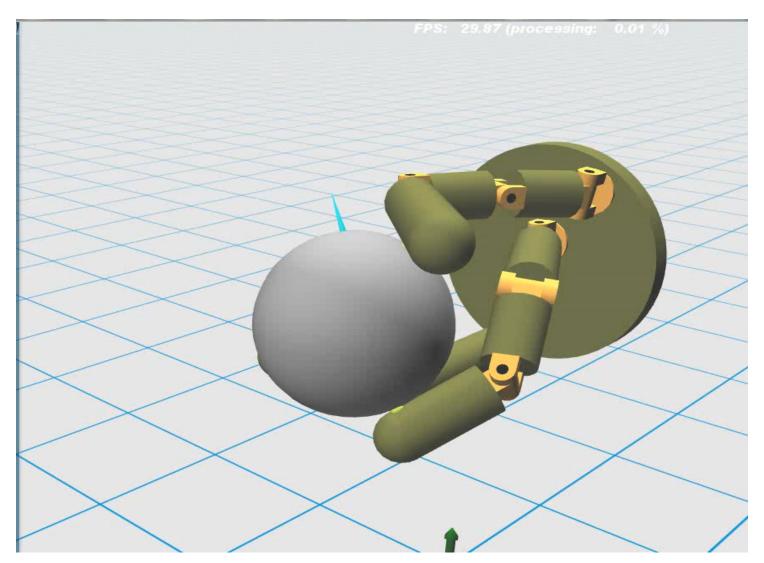
**Sphere Rotation** 

## "Multi-objective" Chaining Example



Sphere Rotation + translation

## "Multi-objective" Chaining Example



Sphere Rotation + xy translation

#### Common Patterns

The mechanisms for each task look totally different!

Non-obvious/non-trivial designs

Different numbers of links for each hand: scales with complexity

Trajectory complexity tends to correspond to importance of fingers

 Hands become more aesthetically pleasing as we add more complexity to motion

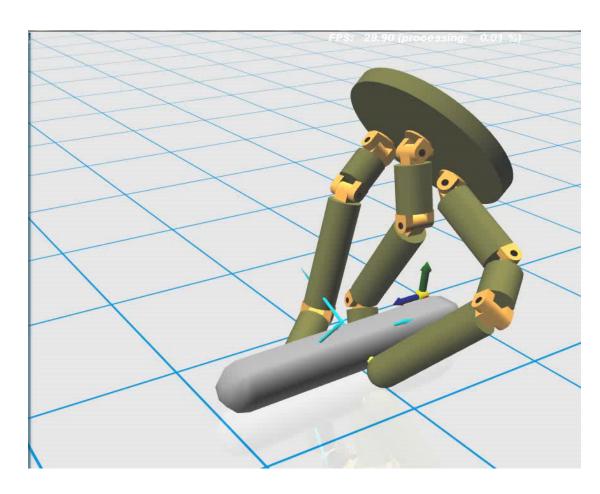
#### Limitations

- Slippage dynamics not exact
  - -discouraged, not prohibited
  - -usually not problematic except at high curvature

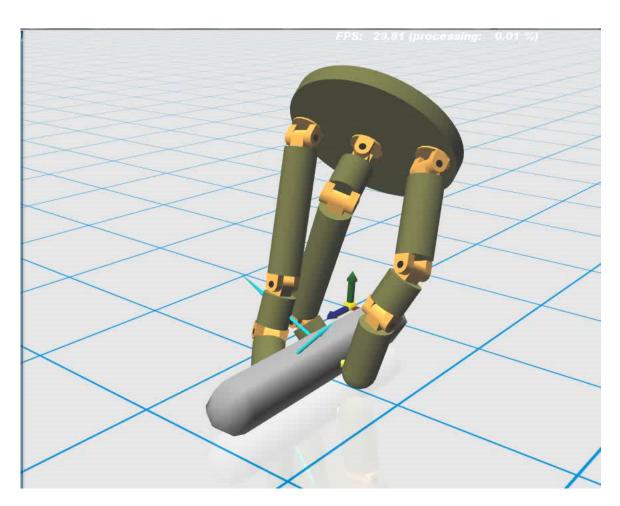
- User must provide a good base position and reasonable initial contacts
  - contacts selected with concept of fingers in mind

- Random contact initialization:
  - -can work but unreliable
  - -disconnect between optimization steps

## Pencil Pickup Slip Demonstration

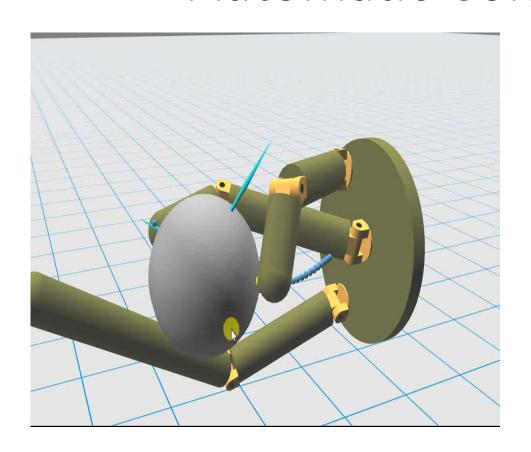


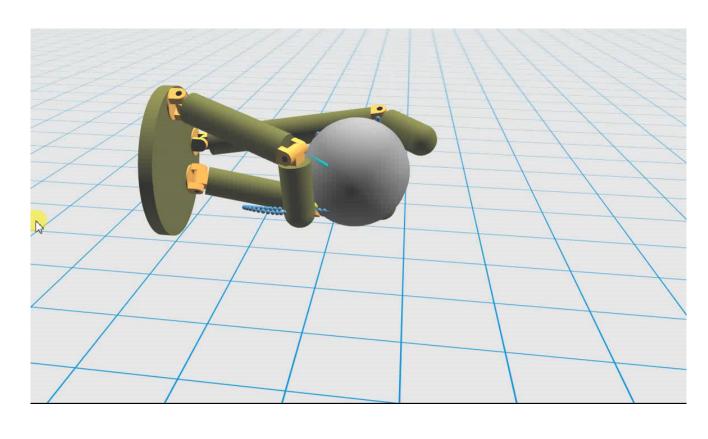
Acceptable Slippage



Uncomfortable Slippage

### Automatic Contact Brittleness Demo





Sphere translate: Ok mechanism

Sphere translate: Brittle mechanism

### Additional Topics For The Future

Multi-objective optimization

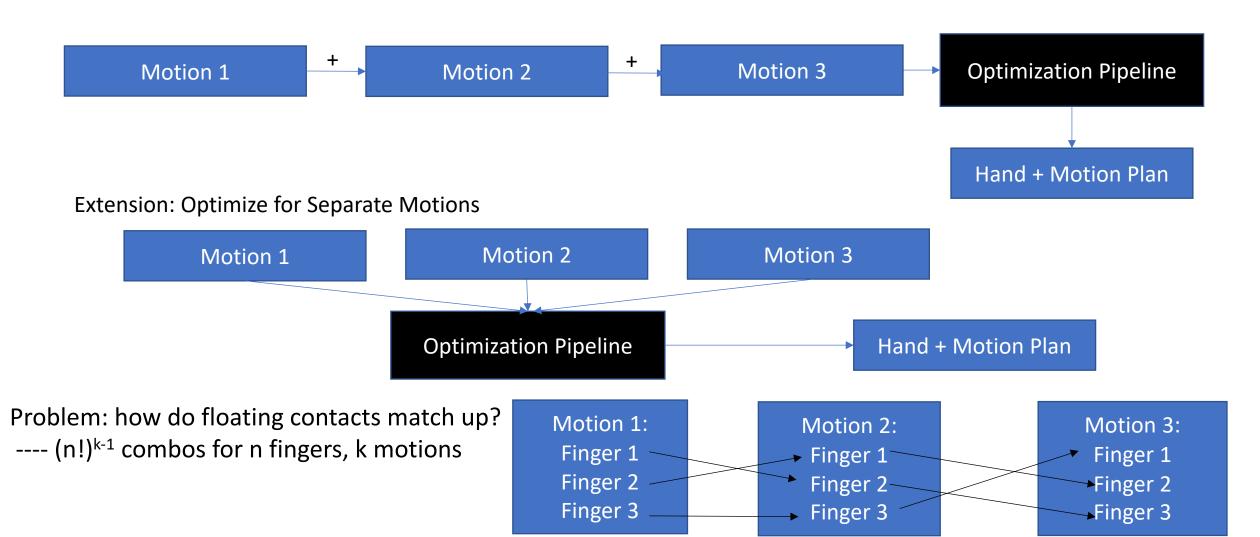
Initial Contact Planning

Robustness through Physical Simulation

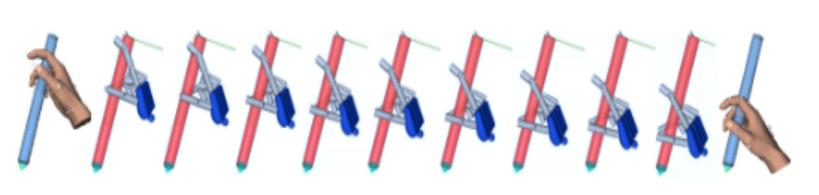
• Incorporating Dimensionality Reduction (Linkages/Synergies)

### Multi-Objective Optimization

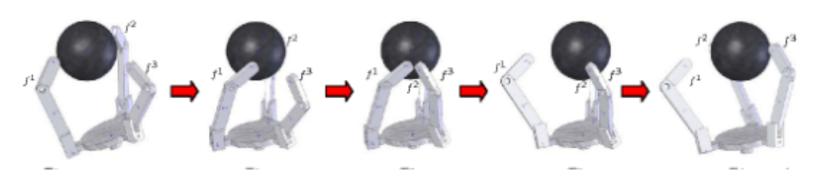
**Current Capability: Motion Chaining** 



## Initial Contact Planning/Additional Floating Heuristics



Vinayavekhin 2011: re-grasp on a cylinder



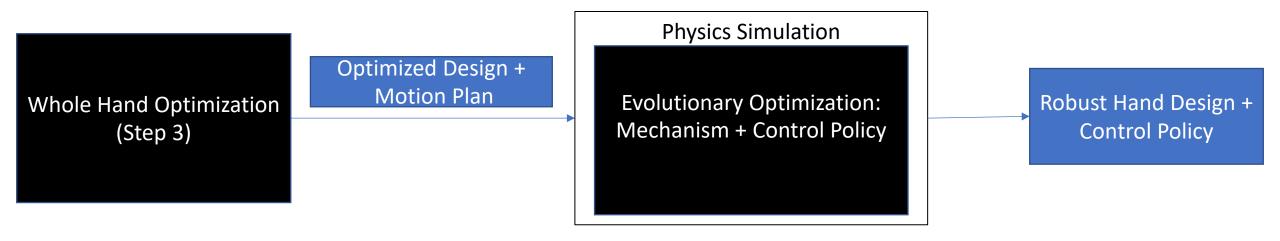
Xu 2007: finger gaiting for sphere rotation



Twirling a pencil

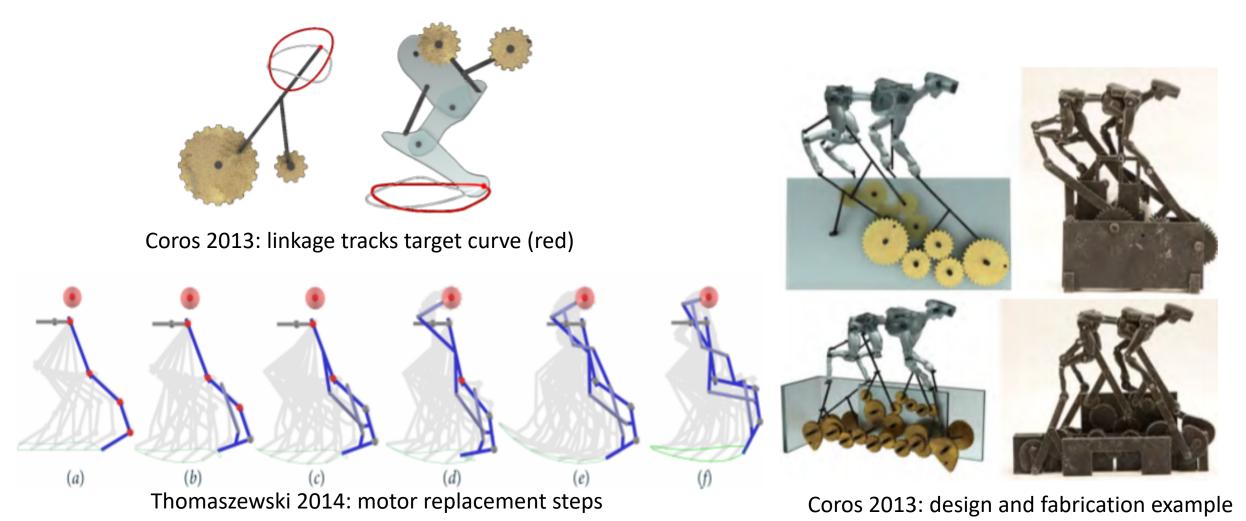
- [1] Finger gaits planning for multifingered manipulation Xu 2007
- [2] Towards an automatic robot regrasping movement ... Vinayavekhin 2011

### Robustness Through Physical Simulation



- Use synthesized mechanism as seed
- Control policy (torque): force feedback or open loop
- Gradient free optimization (e.g. Covariance Matrix Adaptation)
- Final step before fabrication

## Dimensionality Reduction



- [1] "Computational design of mechanical characters" Coros 2013
- [2] "Computational design of linkage-based characters" Thomaszewski 2014